

Gosefnanefnd  
iðnaðarráðuneytisins

EFNASAMSETNING Á PERLUSTEINI Í PRESTAHNÚK

eftir

Gylfa Einarsson

og

Stefán Arnórsson

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## Efnisyfirlit

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## 0. Inngangur.

Efnagreiningarnar í meðfylgjandi skýrslu voru unnar af Gylfa Einarssyni á Jarðfræðistofu Raunvísindastofnunar háskólans undur umsjón Stefáns Arnórssonar og eftir beiðni gosefnanefndar iðnaðarráðuneytisins.

Alls voru 22 sýni efnagreind og voru þau valin af Aðalsteini Jónssyni, Stefáni Arnórssyni og Gylfa Einarssyni úr þeim hópi sýna, sem tekinn var meðan á rannsóknum John-Manville og Perlitnefndar stóð í Prestahnúki sumarið 1971, en þessi sýni hafa verið á geymslu á Rannsóknarstofnun iðnaðarins. Sýnin voru valin með það fyrir augum að viðtækar þensluprófanir yrðu gerðar á þeim auk efnagreininganna.

Tilgangur efnagreininganna var þríþættur:

- (1) Að gera sér sem bezta grein fyrir samsetningu perlusteinsins með samanburði við perlustein, sem er unninn í öðrum löndum.
- (2) Að fá upplýsingar um hversu jöfn (hómógen) efnasamsetningin er í hnúknum.
- (3) Að sjá hver áhrif efnasamsetning hefur á þenslueiginleika og notfæra sér niðurstöður hennar fyrir túlkun á prófunum á forþurrkun og þenslu.

Þessa skýrslu ber að skoða sem framvinduskýrslu, þar sem aðaltilgangurinn er að birta niðurstöður efnagreininga. Mælt er með því að gera lokaskýrslu, þar sem áherzla verður lögð á samanburð efnasamsetningar við þenslueiginleika og útlit perlusteins í þunnsneið.

Númering á sýnum er sú sama og í skýrslu gosefnanefndar: Perlusteinsrannsóknir á Íslandi stutt yfirlit, des. 1972.

## 1. Efnagreiningaraðferðir

$\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{TiO}_2$  og Fe total sem  $\text{Fe}_2\text{O}_3$  var ákvarðað með röntgenfluorence.

FeO var ákvarðað með  $\text{K}_2\text{Cr}_2\text{O}_7$  títrun.

MgO og CaO var ákvarðað með atomic absorption.

$\text{Na}_2\text{O}$  og  $\text{K}_2\text{O}$  var ákvarðað með logafotometer.

MnO og  $\text{P}_2\text{O}_5$  var ákvarðað spektiofotometískt.

$\text{H}_2\text{O}^+$  var ákvarðað gravimetrískt eftir glæðingu.

$\text{H}_2\text{O}^-$  var ákvarðað gravimetrískt eftir þurrkun í 7 klst. við  $105^\circ\text{C}$ .

## 2. Niðurstöður

### 2.1. Skekkjuvaldar

Allmargar af efnagreiningunum hafa of lága summu. Fjórtán liggja ofan við 99 %, sex milli 99 og 98 % og þrjár fyrir neðan 98 %. Þess er helzt að vænta að skekkjan liggi í  $\text{SiO}_2$  - ákvörðun, en ekki var aðstaða til að endurtaka mælingar á  $\text{SiO}_2$  að sinni. Meðaltal af summum þeirra efnagreininga, sem liggja ofan við 99 % er 99,36 %. Meðaltal af  $\text{SiO}_2$  - ákvörðunum er 74,02 %. Meðaltal af summum þeirra efnagreininga, sem liggja neðan við 99 % er hins vegar 98,26 % og meðaltal  $\text{SiO}_2$  - ákvarðana 73,22 %. Bendir þetta til að skekkja í  $\text{SiO}_2$  - ákvörðun eigi stóran þátt í þessari lágu útkomu. Þess ber einnig að gæta, að snefilefni geta verið allt að 0.5 %. Eru þau helztu Ba, Cl, La, Rb, Sr og Zr.

## 2.2 Efnasamsetning perlusteins.

Tafla 1. Meðalefnasamsetning perlusteins í Prestahnúki og skekkjur í efnagreiningu

Meðal % Frávik	Samkvæmni með 95% vissu í %	Meðaltal Efnagr.	Lágmark mark- taks mismunar	spönn einstakra efna
SiO <sub>2</sub>	1.43	73.73	1.05	72.05 - 75.95
Al <sub>2</sub> O <sub>3</sub>	3.19	12.22	0.39	11.76 - 13.03
TiO <sub>2</sub>	4.34	0.13	0.06	0.10 - 0.23
Fe <sub>2</sub> O <sub>3</sub>		0.77		0.60 - 1.02
FeO	4.88	0.81	0.04	0.50 - 1.02
MgO	15.57	0.04	0.01	0.02 - 0.14
CaO	2.68	0.30	0.01	0.20 - 0.41
Na <sub>2</sub> O	15.03	3.94	0.59	3.26 - 4.36
K <sub>2</sub> O	4.10	3.29	0.14	3.09 - 3.60
MnO	38.16	0.01	0.04	0.00 - 0.04
P <sub>2</sub> O <sub>5</sub>	4.38	0.02	0.001	0.02 - 0.04
H <sub>2</sub> O <sub>tot</sub>	31.38	3.73	1.15	1.60 - 5.39
Fe <sub>2</sub> O <sub>3</sub> tot	4.16	1.66	0.07	1.43 - 1.84

Að  $H_2O$  total undanteknu eru tölurnar í tveim fremstu dálkunum fengnar úr skýrslu Einars Gunnlaugssonar og Gests Gíslasonar: "Efnagreiningar á íslenzku basalti vegna hugsanlegrar basaltbræðslu". Þessar tölur eru fengnar við endurteknar greiningar á basalti og eru því ekki algerlega yfirfæranlegar á perlusteini vegna annarrar efnasamsetningar. Útreiknaðar skekkjur fyrir  $H_2O$  total eru fengnar frá endurteknum mælingum á perlusteini.

Í töflu 2 sézt, að lítil breytileiki er í samsetningu perlusteinsins, þó talsvert meiri en nemur marktækum mun og því ekki unnt að segja, að perlusteinninn sé hómógen fyrir öll aðalefni. Heildarefnasamsetningin er æskileg fyrir þenjanlegan perlustein. Líklega mun breytileiki flestra efnanna ekki skipta máli fyrir þenslu-eiginleika perlusteinsins. Undantekningar eru þó  $Na_2O$ ,  $K_2O$  og sér í lagi  $H_2O$ , en styrkur hins síðastnefnda er mjög breytilegur og ætti sá breytileiki að geta haft áhrif á þenslu svo og hvers konar forhitun er nauðsynleg.

### 3. Tillögur um frekari efnarannsóknir

Mælt er með því, að frekari efnarannsóknir feli í sér ákvörðun á  $H_2O$  og  $Na_2O$  og  $K_2O$  og verði síðan reynt að samræma niðurstöður efnagreininganna við þenslueiginleika, útlit í þunnsneið og handstykki. Þessi samanburður ætti að leiða til aukins skilnings á mismunandi þenslueiginleikum einstakra sýna og skapa reynslu til að dæma um þenslueiginleikana eftir útliti handstykkja. Að auki er talið að þessi samanburður veiti vitneskju um það, hvernig perlusteinn myndast, en vatnsinnihald hans er óvenju hátt miðað við annað súrt gosberg.



THE CHEMICAL COMPOSITION OF PERLITE

FROM PRESTAHNÚKUR

by

Gylfi Einarsson

and

Stefán Arnórsson

apríl 1973

## Contents

0. Introduction
1. Analytical techniques
2. Variation in chemical composition
3. Proposals for further chemical studies

## 0. Introduction

The chemical analyses in this report were carried out by Gylfi Einarsson at the Geology Division of the Science Institution under the supervision of Stefán Arnórsson and at the request of the Committee of Volcanic Materials.

Altogether 22 samples were analysed and they were selected by Adalsteinn Jónsson, Stefán Arnórsson, and Gylfi Einarsson from the collection of samples taken during the investigations of Johns Manville and the Perlite Committee in Prestahnúkur during the summer of 1971, but these samples have been stored at the Industrial Research Institute. The samples were selected on the assumption that extensive expansion tests would be carried out on them in addition to the chemical analyses.

The purpose of the analyses was threefold:

- (1) to reveal as well as possible the composition of the perlite and compare it with the composition of exploited perlite in other countries.
- (2) to obtain information on the homogeneity of the perlite in the Prestahnúkur formation.
- (3) to observe the relation between composition and expansion properties of the perlite and apply the results for interpreting expansion tests and pre-heating treatment.

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This report is a preliminary one and its main purpose is to make available the results of the chemical analyses. It is proposed to write a final report where comparison between composition expansion properties, and microscopic character of the perlite will be emphasized.

The sample numbers are those of the report by the Committee on Volcanic Materials: Studies of Perlite in Iceland - a brief review, Dec. 1972.

### 1. Analytical Techniques

$\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{TiO}_2$  and Fe total were determined by X-ray fluorescence.

FeO was determined by HF- $\text{H}_2\text{SO}_4$  solution and  $\text{K}_2\text{Cr}_2\text{O}_7$  titration.

MgO and CaO were determined by atomic absorption .

$\text{Na}_2\text{O}$  and  $\text{K}_2\text{O}$  were determined by flame photometry.

MnO was determined colorimetrically after oxidation to permanganate.

$\text{P}_2\text{O}_5$  was determined colorimetrically by estimation of the molybdate - vanadate complex.

$\text{H}_2\text{O}^+$  was determined gravimetrically after fusion.

$\text{H}_2\text{O}^-$  was determined by drying at  $105^\circ\text{C}$  for 7 hours.

## 2. Results

### 2.1 Sources of error

Several of the analyses have a low sum; 14 have a sum above 99%, 6 between 99 and 98% and 3 below 98%. It is expected that the low sum lies in the  $\text{SiO}_2$  determination but for the time being it was not possible to repeat the measurements. The average of the sums of those analyses which are above 99% is 99.36% and the average  $\text{SiO}_2$  content 74.02%. The average of the sums which are below 99% is on the other hand 98.26% and here the average silica content is 73.22%. This supports the suggestion that the low sum is mostly due to low  $\text{SiO}_2$  values. It should also be pointed out that trace elements can amount to as much as 0.5%. The most important trace elements are Ba, Cl, La, Cb, Sr and Zr.

### 2.2 The composition of the perlite

From table 1 it can be seen that there is little variation in the composition of the perlite. Yet it is considerably higher than analytical error and therefore it cannot be stated that the perlite is homogeneous with respect to all of the major components. The overall composition is desirable for perlite. Probably the variation in the concentration of most of the components will not be significant for expansion properties.  $\text{Na}_2\text{O}$ ,  $\text{K}_2\text{O}$  and in particular  $\text{H}_2\text{O}$  are, however, exceptions, but the  $\text{H}_2\text{O}$  concentrations are very variable and this variability might well influence expansion and the kind of preheating required.

Table 1. The average composition of perlite in Prestahnúkur and analytical errors.

Compound	Mean% deviation	Precision at the 95% c.l.	average compos.	lower limit of sign.diff.	Conc. range
SiO <sub>2</sub>	0.46	1.43	73.73	1.05	72.05-75.95
Al <sub>2</sub> O <sub>3</sub>	1.09	3.19	12.22	0.39	11.76-13.03
TiO <sub>2</sub>	1.54	4.34	0.13	0.06	0.10-0.23
Fe <sub>2</sub> O <sub>3</sub>			0.77		0.60-1.02
FeO	2.22	4.88	0.81	0.04	0.50-1.02
MgO	6.69	15.57	0.04	0.01	0.02-0.14
CaO	1.17	2.68	0.30	0.01	0.20-0.41
Na <sub>2</sub> O	5.28	15.03	3.94	0.59	3.26-4.36
K <sub>2</sub> O	1.25	4.10	3.29	0.14	3.08-3.60
MnO	16.05	38.16	0.01	0.04	0.00-0.04
P <sub>2</sub> O <sub>5</sub>	1.12	4.38	0.02	0.001	0.02-0.04
H <sub>2</sub> O <sub>tot.</sub>	9.70	31.38	3.73	1.15	1.60-5.39
Fe <sub>2</sub> O <sub>3</sub> <sub>tot.</sub>	1.56	4.16	1.66	0.07	1.43-1.84

With the exception of H<sub>2</sub>O total the figures in the 2 first columns have been obtained from a report on basalt casting by Einar Gunnlaugsson and Gestur Gíslason. These figures were derived from duplicate analyses of basalt and are not directly applicable for perlite because of difference in composition. The calculated error for H<sub>2</sub>O total were obtained by duplicate analyses of perlite.

### 3. Proposals for further chemical studies

It is recommended that further chemical studies involve analyses of  $H_2O$ ,  $Na_2O$  and  $K_2O$  and correlation between chemical composition, expansion properties, microscopic characteristics and hand specimen be attempted. This correlation should improve understanding regarding variable expansion properties of individual samples and should create experience to judge expansion properties according to the outlook of hand specimens. In addition, it is believed, that this correlation increase knowledge about how perlite may form, but its water content is unusually high compared with other acid volcanic glasses.

SI02 73.35 73.44  
 AL20 12.28 7.24  
 T102 .14 .10  
 FE20 .81 .30  
 FE0 .93 .77  
 MND .03 .02  
 MGO .02 .02  
 CAU .38 .40  
 NA20 4.36 4.23  
 K20 3.42 2.18  
 P205 .03 .01  
 H2O 3.36 11.23  
 H2O 99.11 100.00

H<sub>2</sub>O<sup>+</sup> : 3.25

H<sub>2</sub>O<sup>-</sup> : 0.11

QZ 33.68  
 OR 20.21  
 AB 36.89  
 AN 1.70  
 LC 0.00  
 NE 0.00  
 CD 0.00  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .04  
 FS .86  
 FO 0.00  
 FA 0.00  
 MT 1.17  
 IM .26  
 HM 0.00  
 AP .06  
 RT 0.00  
 VN 3.35  
 98.28

A 82.2 DI 0.0  
 F 17.5 QZ 97.3  
 M .2 HY 2.6

FE203/FE0 .87096

OR 34.3 QZ 37.1  
 AB 62.7 OR 22.2  
 AN 2.9 AB 40.6



SI02	73.80	73.30
AL20	12.14	7.10
TI02	.10	.07
FE20	.99	.37
FED	.72	.59
HND	0.00	0.00
MGU	.04	.05
CAU	.32	.34
NA20	3.82	3.67
K20	3.60	2.28
P205	.03	.01
H20	3.67	12.16
	99.23	100.00

H<sub>2</sub>O<sup>+</sup> : 3.46

H<sub>2</sub>O<sup>-</sup> : 0.21

QZ	36.92
OR	21.27
AB	32.32
AN	1.41
LC	0.00
NE	0.00
CO	.01
WD	0.00
EN	0.00
FS	0.00
EN	.09
FSS	.33
FO	0.00
FA	0.00
MT	1.43
IM	.18
HM	0.00
AP	.06
RT	0.00
VN	3.66
	97.74

A	81.7	DI	0.0
F	17.7	QZ	98.8
M	.4	HY	1.1

FE203/FED 1.37500

UR	38.6	QZ	40.7
AB	58.7	OR	23.5
AN	2.5	AB	35.7

SI02	73.45	69.51
AL20	11.95	6.66
TI02	.10	.07
FE20	.67	.23
FEU	.87	.68
MANO	0.00	0.00
MGO	.04	.05
CAO	.38	.38
NA20	3.88	3.56
K20	3.10	1.87
P205	.02	0.00
H2O	5.36	16.93
	99.82	100.00

H<sub>2</sub>O<sup>+</sup> : 5.29

H<sub>2</sub>O<sup>-</sup> : 0.07

QZ	37.73
OR	18.31
AB	32.83
AN	1.76
LC	0.00
NE	0.00
CD	.01
WD	0.00
EN	0.00
FS	0.00
EN	.09
FSS	.87
FD	0.00
FA	0.00
MT	.97
IM	.18
HM	0.00
AP	.04
RT	0.00
VN	5.35
	98.21

A	82.1	DI	0.0
F	17.3	QZ	97.4
M	.4	HY	2.5

FE203/FEU .77011

OR	34.6	QZ	42.4
AB	62.0	OR	20.5
AN	3.3	AB	36.9

SI02	75.95	78.90
AL20	12.15	7.43
TI02	.12	.09
FE20	.67	.26
FED	.92	.79
MND	0.00	0.00
MGD	.02	.03
CA0	.30	.33
NA20	4.26	4.29
K20	3.46	2.29
P205	.02	0.00
H20	1.60	5.54
	99.47	100.00

H<sub>2</sub>O<sup>+</sup> : 1.50

H<sub>2</sub>O<sup>-</sup> : 0.10

QZ	36.82
OR	20.44
AB	36.04
AN	1.37
LC	0.00
NE	0.00
CO	0.00
WD	0.00
EN	0.00
FS	0.00
EN	.04
FS	.93
FO	0.00
FA	0.00
MT	.97
IM	.22
HM	0.00
AP	.04
RT	0.00
VN	1.59
	98.52

A	83.3	DI	0.0
F	16.4	QZ	97.3
M	.2	HY	2.6

FE203/FEU .72826

OR	35.3	QZ	39.4
AB	62.2	OR	21.9
AN	2.3	AB	38.6

S102	73.85	71.49
AL20	11.95	6.81
TI02	.13	.09
FE20	.61	.22
FE0	.83	.67
MND	.03	.02
MGO	.03	.04
CA0	.20	.20
NA20	4.12	3.86
K20	3.30	2.03
P205	.02	0.00
H20	4.49	14.51
	99.56	100.00

H<sub>2</sub>O<sup>+</sup> : 4.22

H<sub>2</sub>O<sup>-</sup> : 0.27

QZ	36.38
DR	19.50
AB	34.86
AN	.87
LC	0.00
NE	0.00
CO	.01
WD	0.00
EN	0.00
FS	0.00
EM	.07
FSS	.86
FO	0.00
FA	0.00
MT	.68
IM	.24
HM	0.00
AP	.04
RT	0.00
VN	4.48
	98.23

FE203/FE0 .73493

A	84.0	DI	0.0
F	15.6	QZ	97.4
M	.3	HY	2.5

OR	35.3	QZ	40.0
AB	63.1	OR	21.4
AN	1.5	AB	38.4

SI02	73.65	71.78
AL20	11.97	6.87
TI02	.23	.16
FE20	1.02	.37
FE0	.50	.40
MND	0.00	0.00
MGO	.14	.20
CA0	.32	.33
NA20	3.41	3.22
K20	3.23	2.00
P205	.04	.01
H20	4.49	14.60
	99.00	100.00

H<sub>2</sub>O<sup>+</sup> : 3.89

H<sub>2</sub>O<sup>-</sup> : 0.60

QZ	40.59
OR	19.08
AB	28.85
AN	1.35
LC	0.00
NE	0.00
CO	.02
WD	0.00
EN	0.00
FS	0.00
EN	.34
FS	0.00
FD	0.00
FA	0.00
HT	.94
IM	.43
HM	.36
AP	.08
RT	0.00
VN	4.48
	96.59

A	80.9	DI	0.0
F	17.2	QZ	99.1
M	1.7	HY	.8

FE203/FEU 2.04000

OR	38.7	QZ	45.8
AB	58.5	OR	21.5
AN	2.7	AB	32.5

S102 74.40 77.21  
 AL20 13.03 7.96  
 T102 .14 .10  
 FE20 .84 .32  
 FEU .84 .72  
 MND 0.00 0.00  
 MGD .02 .03  
 CAD .20 .22  
 NA20 4.02 4.04  
 K20 3.12 2.06  
 P205 .02 0.00  
 H2O 3.10 7.27  
 99.73 100.00

$H_2O^+$  : 2.93  
 $H_2O^-$  : 0.17

QZ 38.32  
 OR 18.43  
 AB 34.01  
 AN .87  
 LC 0.00  
 NE 0.00  
 CO .02  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .04  
 FS .61  
 FO 0.00  
 FA 0.00  
 MT 1.21  
 IM .26  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 2.09  
 95.97

A 81.5 DI 0.0  
 F 18.2 QZ 98.2  
 M .2 HY 1.7

FE203/FEU 1.00000

OR 34.5 QZ 42.2  
 AB 63.7 OR 20.3  
 AN 1.6 AB 37.4

SI02	74.05	72.39
AL20	12.32	7.09
T102	.13	.09
FE20	.78	.28
FED	.78	.63
MND	.04	.03
MGO	.02	.02
CAO	.35	.36
NA20	3.68	3.48
K20	3.24	2.02
P205	.02	0.00
H20	4.15	13.54
	99.56	100.00

H<sub>2</sub>O<sup>+</sup> : 3.90

H<sub>2</sub>O<sup>-</sup> : 0.25

QZ	39.15
OR	19.14
AR	31.13
AN	1.61
LC	0.00
NE	0.00
CO	.02
WD	0.00
EN	0.00
FSS	0.00
EN	.04
FSS	.64
FD	0.00
FA	0.00
MT	1.13
IM	.24
HM	0.00
AP	.04
RT	0.00
VN	4.14
	97.35

A	82.1	DI	0.0
F	17.5	QZ	98.2
M	.2	HY	1.7

FE203/FED 1.00000

OR	36.8	QZ	43.7
AB	59.9	OR	21.4
AN	3.1	AB	34.8

S102 74.35  
 AL20 12.14  
 T102 .12  
 FE20 1.00  
 FED .64  
 MND .03  
 MGD .02  
 CAO .32  
 NA20 4.22  
 K20 3.60  
 P205 .02  
 H20 2.89  
 99.35

75.14  
 7.23  
 .09  
 .38  
 .54  
 .02  
 .03  
 .34  
 4.13  
 2.32  
 0.00  
 9.75  
 100.00

H<sub>2</sub>O<sup>+</sup> : 2.67

H<sub>2</sub>O<sup>-</sup> : 0.22

QZ 35.21  
 OR 21.27  
 AB 35.70  
 AN 1.46  
 LC 0.00  
 NE 0.00  
 CD 0.00  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .04  
 FS .20  
 FO 0.00  
 FA 0.00  
 MT 1.44  
 IM .22  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 2.88  
 98.54

FE203/FED 1.56250

A 83.3  
 F 16.4  
 M .2  
 DI 0.0  
 QZ 99.2  
 HY .7

OR 36.3  
 AB 61.0  
 AN 2.5  
 QZ 38.1  
 OR 23.0  
 AB 38.7



SI02	74.25	72.52
AL20	11.95	6.87
TI02	.15	.11
FE20	.89	.32
FEO	.59	.48
MND	0.00	0.00
MGD	.10	.14
CAO	.20	.20
NA20	4.02	3.80
K20	3.28	2.04
P205	.02	0.00
H20	4.13	13.46
	99.58	100.00

H<sub>2</sub>O<sup>+</sup> : 3.58

H<sub>2</sub>O<sup>-</sup> : 0.55

QZ	37.68
DR	19.38
AB	34.01
AN	.87
LC	0.00
NE	0.00
CO	.01
WD	0.00
EN	0.00
FS	0.00
EN	.24
FSS	.10
FO	0.00
FA	0.00
MT	1.29
IM	.28
HM	0.00
AP	.04
RT	0.00
VN	4.12
	98.06

A	83.0	DI	0.0
F	15.8	QZ	99.0
M	1.1	HY	.9

FE203/FEU 1.50847

OR	35.7	QZ	41.3
AB	62.6	OR	21.2
AN	1.6	AB	37.3

SID2 73.40 74.51  
 AL20 11.95 7.15  
 TID2 .12 .09  
 FE20 .65 .24  
 FEU .94 .79  
 MND 0.00 0.00  
 MGO .02 .03  
 CAD .23 .25  
 NA20 3.88 3.81  
 K20 3.30 2.13  
 P205 .02 0.00  
 H2O 3.23 10.94  
 97.74 100.00

H<sub>2</sub>O<sup>+</sup> : 3.13

H<sub>2</sub>O<sup>-</sup> : 0.10

QZ 37.22  
 OR 19.50  
 AB 32.83  
 AN 1.02  
 LC 0.00  
 NE 0.00  
 CO .01  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .04  
 FS .99  
 FO 0.00  
 FA 0.00  
 MT .94  
 IM .22  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 3.22  
 96.07

FE203/FEU .69148

A 82.2 DI 0.0  
 F 17.4 QZ 97.2  
 M .2 HY 2.7

OR 36.5 QZ 41.5  
 AB 61.5 OR 21.7  
 AN 1.9 AB 36.6

S102	73.85	73.22
AL20	12.12	7.08
T102	.14	.10
FE20	.87	.32
FED	.75	.62
MND	.03	.02
MGD	.03	.04
CAO	.23	.24
NA20	3.98	3.82
K20	3.14	1.98
P205	.02	0.00
H20	3.78	12.51
	98.94	100.00

H<sub>2</sub>O<sup>+</sup> : 3.62

H<sub>2</sub>O<sup>-</sup> : 0.16

QZ	37.91
DR	18.55
AB	33.67
AN	1.02
LC	0.00
NE	0.00
CJ	.01
WD	0.00
EN	0.00
F S	0.00
EN	.07
F S	.48
FO	0.00
FA	0.00
WT	1.26
IM	.26
HM	0.00
AP	.04
RT	0.00
VN	3.78
	97.10

A	81.9	DI	0.0
F	17.6	QZ	98.5
M	.3	HY	1.4

FEE203/FED 1.16000

DR	34.8	QZ	42.0
AB	63.2	DR	20.5
AN	1.9	AB	37.3

S102	72.05	69.51
AL20	11.98	6.81
T102	.10	.07
FE20	.64	.23
FED	.71	.57
MNG	0.00	0.00
MGO	.05	.07
CAO	.29	.29
NA20	3.26	3.04
K20	3.26	2.00
P205	.03	.01
H2O	5.39	17.35
	97.76	100.00

H<sub>2</sub>O<sup>+</sup> : 5.06

H<sub>2</sub>O<sup>-</sup> : 0.33

QZ	39.65
DR	19.26
AB	27.58
AN	1.26
LC	0.00
NE	0.00
CD	.02
WD	0.00
EN	0.00
F S	0.00
EN	.12
F S	.60
FD	0.00
FA	0.00
MT	.92
IM	.18
HM	0.00
AP	.06
RT	0.00
VN	5.38
	95.09

A	82.9	DI	0.0
F	16.3	QZ	98.1
M	.6	HY	1.8

FE203/FED .90140

DR	40.0	QZ	45.8
AB	57.3	DR	22.2
AN	2.6	AB	31.8

S102 74.25  
 AL20 12.22  
 T102 .13  
 FE20 .81  
 FED .82  
 MND .03  
 MGO .02  
 CAO .35  
 NA20 4.00  
 K20 3.28  
 P205 .02  
 H20 2.98  
 98.91

75.07  
 7.28  
 .09  
 .30  
 .69  
 .02  
 .03  
 .37  
 3.92  
 2.11  
 0.00  
 10.05  
 100.00

$H_2O^+$  : 2.76  
 $H_2O^-$  : 0.22

QZ 37.33  
 OR 19.38  
 AB 33.84  
 AN 1.61  
 LC 0.00  
 NE 0.00  
 CD .01  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .04  
 FS .67  
 FO 0.00  
 FA 0.00  
 MT 1.17  
 IM .24  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 2.97  
 97.37

FE203/FEU .98780

A 82.2  
 F 17.5  
 M .2  
 DI 0.0  
 QZ 98.0  
 HY 1.9

OR 35.3  
 AB 61.7  
 AN 2.9  
 QZ 41.2  
 OR 21.4  
 AB 37.3

S102 74.00 72.16  
 AL20 11.76 6.75  
 T102 .11 .08  
 FE20 .66 .24  
 FE0 .73 .59  
 MN0 0.00 0.00  
 MG0 .04 .05  
 CA0 .26 .27  
 NA20 3.98 3.76  
 K20 3.42 2.12  
 P205 .02 0.00  
 H20 4.28 13.93  
 99.26 100.00

$H_2O^+$  : 4.08  
 $H_2O^-$  : 0.20

QZ 36.85  
 OR 20.21  
 AB 33.67  
 AN 1.17  
 LC 0.00  
 NE 0.00  
 CO .01  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .09  
 FS .61  
 FO 0.00  
 FA 0.00  
 MT .95  
 IM .20  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 4.27  
 98.13

FE203/FE0 .90410

A 84.4 DI 0.0  
 F 15.1 QZ 98.1  
 M .4 HY 1.8

OR 36.7 QZ 40.6  
 AB 61.1 OR 22.2  
 AN 2.1 AB 37.1

S102 73.40  
 AL20 12.03  
 T102 .12  
 FE20 .77  
 FEU .77  
 MNO 0.00  
 MGO .04  
 CAO .26  
 NA20 3.88  
 K20 3.08  
 P205 .04  
 H2O 3.82  
 H2O 98.21

73.14  
 7.06  
 .08  
 .28  
 .64  
 0.00  
 .05  
 .27  
 3.74  
 1.95  
 .01  
 12.70  
 100.00

$H_2O^+$  : 3.50  
 $H_2O^-$  : 0.32

QZ 38.20  
 DR 18.20  
 AB 32.83  
 AN 1.05  
 LC 0.00  
 NE 0.00  
 CD .01  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .09  
 FS .57  
 FD 0.00  
 FA 0.00  
 MT 1.11  
 IM .22  
 HM 0.00  
 AP .08  
 RT 0.00  
 VN 3.81  
 96.24

A 82.2  
 F 17.2  
 M .4

DI 0.0  
 QZ 98.2  
 HY 1.7

FE203/FEU 1.00000

OR 34.9  
 AB 63.0  
 AN 2.0

QZ 42.8  
 OR 20.3  
 AB 36.7

S102 73.80 72.52  
 AL20 12.32 7.13  
 T102 .11 .08  
 FE20 .60 .22  
 FED .96 .78  
 MND 0.00 0.00  
 MGD .03 .04  
 CAO .23 .24  
 NA20 4.00 3.81  
 K20 3.16 1.98  
 P205 .02 0.00  
 H20 4.01 13.15  
 99.24 100.00

$H_2O^+$  : 3.86  
 $H_2O^-$  : 0.15

QZ 37.40  
 OR 18.67  
 AB 33.84  
 AN 1.02  
 LC 0.00  
 NE 0.00  
 CD .01  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .07  
 FS 1.08  
 FD 0.00  
 FA 0.00  
 MT .86  
 IM .20  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 4.00  
 97.25

FE203/FED .62500

A 82.3 DI 0.0  
 F 17.2 QZ 96.9  
 M .3 HY 3.0

OR 34.8 QZ 41.5  
 AB 63.2 OR 20.7  
 AN 1.9 AB 37.6



SI02	74.27	75.21
AL20	12.31	7.34
T102	.11	.08
FE20	.73	.27
FE0	.79	.66
MND	0.00	0.00
MGO	.04	.06
CAO	.41	.44
NA20	4.22	4.14
K20	3.48	2.24
P205	.02	0.00
H20	2.81	9.50
	99.19	100.00

H<sub>2</sub>O<sup>+</sup> : 2.77

H<sub>2</sub>O<sup>-</sup> : 0.04

A	83.8	DI	0.0
F	15.7	QZ	97.8
M	.4	HY	2.1

OR	35.3
AB	61.3
AN	3.2

QZ	38.4
OR	22.4
AB	39.0

QZ	35.15
OR	20.56
AB	35.70
AN	1.91
LC	0.00
NE	0.00
CO	0.00
WD	0.00
EN	0.00
FS	0.00
EN	.09
FS	.66
FO	0.00
FA	0.00
MT	1.05
IM	.20
HM	0.00
AP	.04
RT	0.00
VN	2.80
	98.24

FE203/FEU .92405

S102 72.32 72.89  
 AL20 13.07 7.76  
 T102 .11 .08  
 FE20 .76 .28  
 FED .79 .66  
 MNDO 0.00 0.00  
 MGD .02 .03  
 CAU .38 .41  
 NA20 4.02 3.92  
 K20 3.24 2.08  
 P205 .02 0.00  
 H2O 3.52 11.84  
 98.25 100.00

QZ 35.39  
 OR 19.14  
 AB 34.01  
 AN 1.76  
 LC 0.00  
 NE 0.00  
 CO .02  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .04  
 FS .64  
 FO 0.00  
 FA 0.00  
 MT 1.10  
 IM .20  
 HM 0.00  
 AP .04  
 RT 0.00  
 VN 3.51  
 95.91

H<sub>2</sub>O<sup>+</sup> : 3.29

H<sub>2</sub>O<sup>-</sup> : 0.23

A 82.9 DI 0.0  
 F 16.8 QZ 98.0  
 M .2 HY 1.9

FE203/FED .96202

OR 34.8 QZ 39.9  
 AB 61.9 OR 21.6  
 AN 3.2 AB 38.4

S102 72.47  
 AL20 12.26  
 T102 .12  
 FE20 .73  
 FED .88  
 MND .03  
 MGD .03  
 CAO .35  
 NA20 3.82  
 K20 3.30  
 P205 .03  
 H2O 4.30  
 98.32

71.45  
 7.12  
 .08  
 .27  
 .72  
 .02  
 .04  
 .36  
 3.65  
 2.07  
 .01  
 14.15  
 100.00

$H_2O^+$  : 4.1  
 $H_2O^-$  : 0.1

QZ 36.44  
 UR 19.50  
 AB 32.32  
 AN 1.55  
 LC 0.00  
 NE 0.00  
 CO .01  
 WD 0.00  
 EN 0.00  
 FS 0.00  
 EN .07  
 FS .87  
 FD 0.00  
 FA 0.00  
 MT 1.05  
 IM .22  
 HM 0.00  
 AP .06  
 RT 0.00  
 VN 4.29  
 96.44

A 81.9 DI 0.0  
 F 17.6 QZ 97.4  
 M .3 HY 2.5

FE203/FED .82954

OR 36.5 QZ 41.2  
 AB 60.5 UR 22.0  
 AN 2.9 AB 36.6

SIU2 74.00 76.71  
 AL20 12.30 7.51  
 TI02 .12 .09  
 FE20 .72 .28  
 FEU .93 .80  
 MND 0.00 0.00  
 MGD .03 .04  
 CAD .29 .32  
 MA20 3.98 4.00  
 K20 3.18 2.10  
 P205 .04 .01  
 H2O 2.34 8.09  
 97.93 100.00

H<sub>2</sub>O<sup>+</sup> : 2.19  
 H<sub>2</sub>O<sup>-</sup> : 0.15

QZ 37.63  
 DR 18.79  
 AB 33.67  
 AN 1.20  
 LC 0.00  
 NE 0.00  
 CO .01  
 MO 0.00  
 EN 0.00  
 FS 0.00  
 EN .07  
 FS .91  
 FO 0.00  
 FA 0.00  
 WT 1.04  
 IM .22  
 HM 0.00  
 AP .08  
 RT 0.00  
 VN 2.34  
 96.01

A 81.6 DI 0.0  
 F 17.9 QZ 97.4  
 M .3 HY 2.5

FE203/FEU .77419

OR 35.0 QZ 41.7  
 AB 62.7 OR 20.8  
 AN 2.2 AB 37.3

S102	73.20	71.95
AL20	12.60	7.29
T102	.12	.08
FE20	.62	.22
FEU	1.02	.83
MND	0.00	0.00
MGO	.03	.04
CAO	.29	.30
NA20	3.78	3.60
K20	3.16	1.98
P205	.02	0.00
H20	4.16	13.65
	99.00	100.00

H<sub>2</sub>O<sup>+</sup> : 4.00  
H<sub>2</sub>O<sup>-</sup> : 0.16

QZ	37.91
DR	18.67
AR	31.98
AN	1.32
LC	0.00
NE	0.00
CD	.02
WD	0.00
EN	0.00
FSS	0.00
EN	.07
FSS	1.16
FO	0.00
FA	0.00
MT	.89
IM	.22
HMI	0.00
AP	.04
RT	0.00
VN	4.15
	96.48

A	81.1	DI	0.0
F	18.4	QZ	96.8
M	.3	HY	3.1

FE203/FEU .60784

QR	35.9	QZ	42.8
AR	61.5	JR	21.0
AN	2.5	AB	36.1